

**CEOP/IGWCO Meeting, Feb. 28th ~ March 3rd 2005, Tokyo**

**Hydrological Improvement of  
the Land Surface Process Scheme Using  
the CEOP Observation**

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# **Contents:**

- 1. Requirement from the hydrological applications**
- 2. A hydrologically enhanced land-surface process model**
- 3. Model validation using the CEOP data**
- 4. Conclusion**

## Atmospheric Models

- Numerical Weather Prediction
- Climate change

## Fluxes

- Net radiation
- LE, H, G
- CO<sub>2</sub>, CH<sub>4</sub>

## Forcing

- Precipitation
- Radiation
- T, u, q

## Land Surface Models

- Water-Energy-Carbon Cycle
- Hydrological Model

## **Water Resources Management**

- water availability, ● water quality, ● water consumption

# Several Urgent Issues in Hydrological Application

- **Impacts of human activity to the hydrological processes and its induced spatial and temporal variability of water resources.**
- **Hydrological responses to the climate changes and its induces possible variability in water resources.**
- **Role of vegetation in the hydrological cycle for the integrated basin management.**
- **Managing water quality together with water quantity.**

# The Distributed Hydrological Model

## On the Basin Scale

- River flow routing
- Groundwater flow

**Basin Scale**  
(regional scale)

Scaling-up

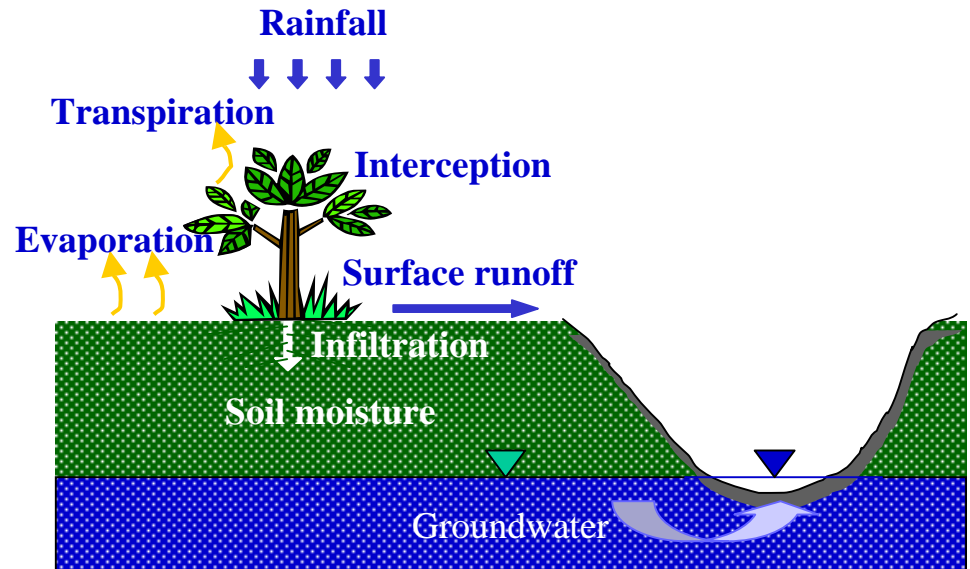
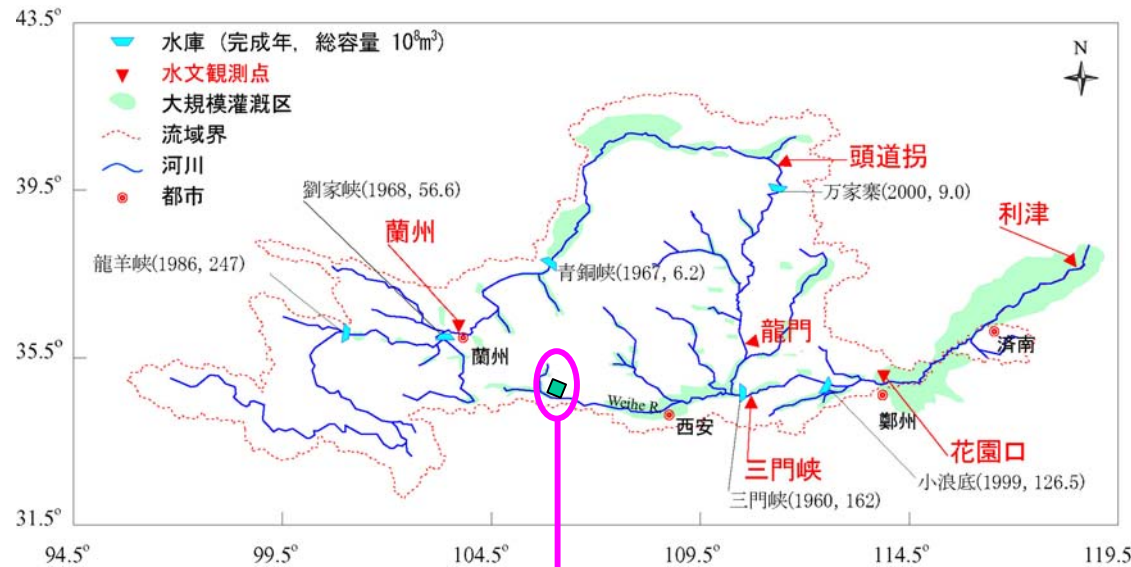


**Model Structure**

**Hillslope Scale**  
(field scale)

## On the Hillslope (field) Scale

- Hydrological Processes: rainfall-infiltration-runoff
- Potential  $E_p \rightarrow$  Actual  $E_a$



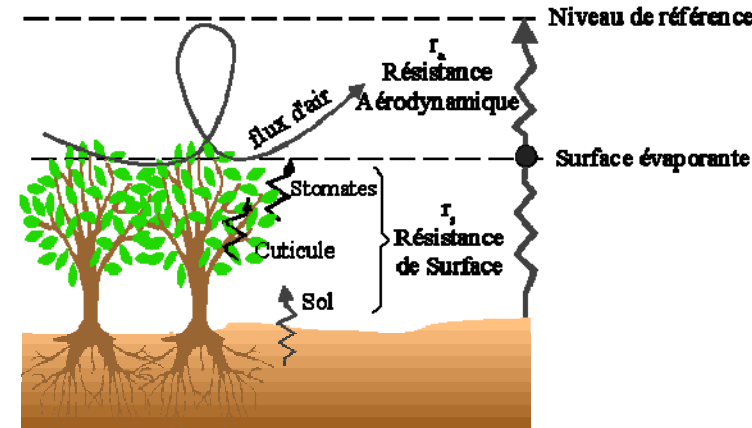
# *Net radiation → potential evaporation → actual evapotranspiration*

**Penman equation** for potential evaporation:

$$E = \frac{\Delta}{\lambda(\Delta + \gamma)} (R_n - G) + \frac{\rho c_a (e_s - e_{za}) / r_a}{\lambda(\Delta + \gamma)}$$

**Penman-Monteith equation** for the actual evapotranspiration:

$$E_a = \frac{\Delta(R_n - G) + \rho c_a (e_s - e_{za}) / r_a}{\lambda[\Delta + \gamma(1 + \frac{r_s}{r_a})]}$$



**Reference crop evaporation:**

$r_s = 70 \text{ s/m}$ ,  $r_a = 208/u_2 \text{ s/m}$ , the Penman-Monteith equation become:

$$E_{rc} = \frac{0.408\Delta(R_n - G) + \gamma \frac{900}{T + 273} (e_s - e_{za}) u_2}{\Delta + \gamma(1 + 0.34u_2)}$$

**Net Radiation:**  $R_n = S_n + L_n$

$$S_n = S_t(1 - \alpha)$$

$$S_t = \left( a_s + b_s \frac{n}{N} \right) S_0$$

$$S_0 = 15.392 d_r (\omega_s \sin \phi \sin \delta + \cos \phi \cos \delta \sin \omega_s)$$

$$L_n = -f \varepsilon' \sigma (T_a + 273.15)^4 / (\lambda \rho_w \cdot 10^{-3})$$

$$f = \left( a_c \frac{b_s}{a_s + b_s} \right) \frac{n}{N} + \left( b_c + \frac{a_s}{a_s + b_s} a_c \right)$$

$$\varepsilon' = a_e + b_e \sqrt{e_d}$$

### Parameters:

(1) albedo ( $\alpha$ ): seasonal and regional characteristics

(2)  $a_s, b_s, a_c, b_c, a_e, b_e$ : with regional characteristics

# *Actual Evapotranspiration*

*(Kristensen and Jensen 1975)*

Calculating the actual transpiration  $E_{at}$  as :

$$E_t = f_{(\theta)}^1 f_{(LAI)} f_{(RDF)} E_{rc}$$

$$\begin{cases} f_{(LAI)} = C_2 + C_1 LAI \rightarrow \text{if } \cdot LAI < \frac{(1-C_2)}{C_1} & \{C_1, C_2 \text{ are constants}\} \\ f_{(LAI)} = 1 \rightarrow \text{else} \end{cases}$$

$$f_{(\theta)}^1 = 1 - \left( \frac{\theta_f - \theta}{\theta_f - \theta_w} \right)^{\frac{C_3}{E_{rc}}}$$

$C_3$  :empirical parameter(mm/day)

$\theta_f$ : volumetric moisture content at field capacity

$\theta_w$ : volumetric moisture content at wilting point

$\theta$ : volumetric moisture content of the layer

And actual evaporation from upper layer  $E_s$  as:

$$E_s = (E_{rc} - E_t) f_{(\theta)}^1$$



# *Infiltration and Unsaturated Zone*

## **Governing Equation for 1-D Flow**

Momentum Equation (Darcy's law)

$$q = -K(\theta) \frac{d(\psi + z)}{dz}$$

Continuity equation

$$\frac{\partial \theta}{\partial t} = -\frac{\partial q}{\partial z}$$

By combining them, **Richards' equation** is obtained

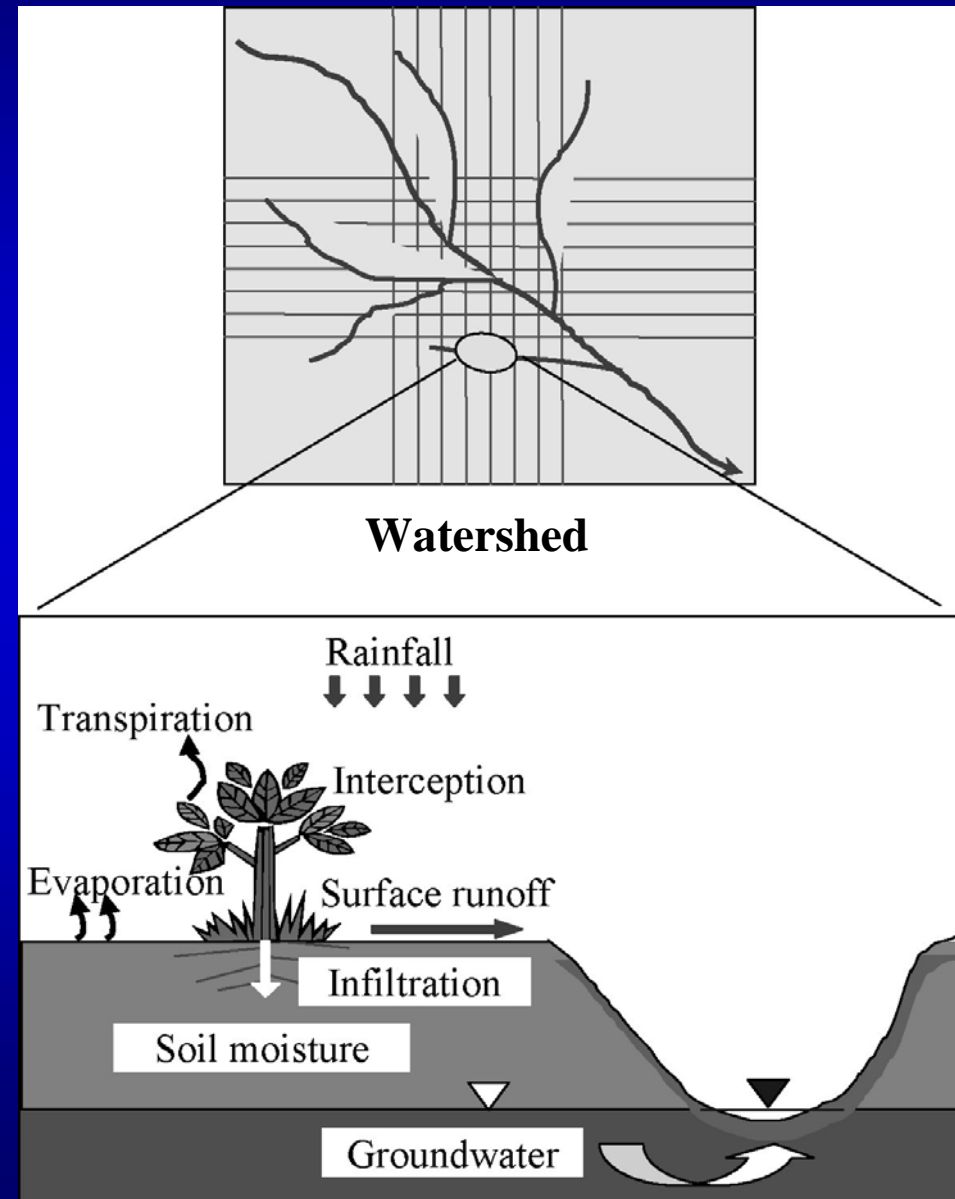
$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left\{ K(\theta) \frac{\delta \psi}{\delta z} + 1 \right\}$$

### *Soil-water properties:*

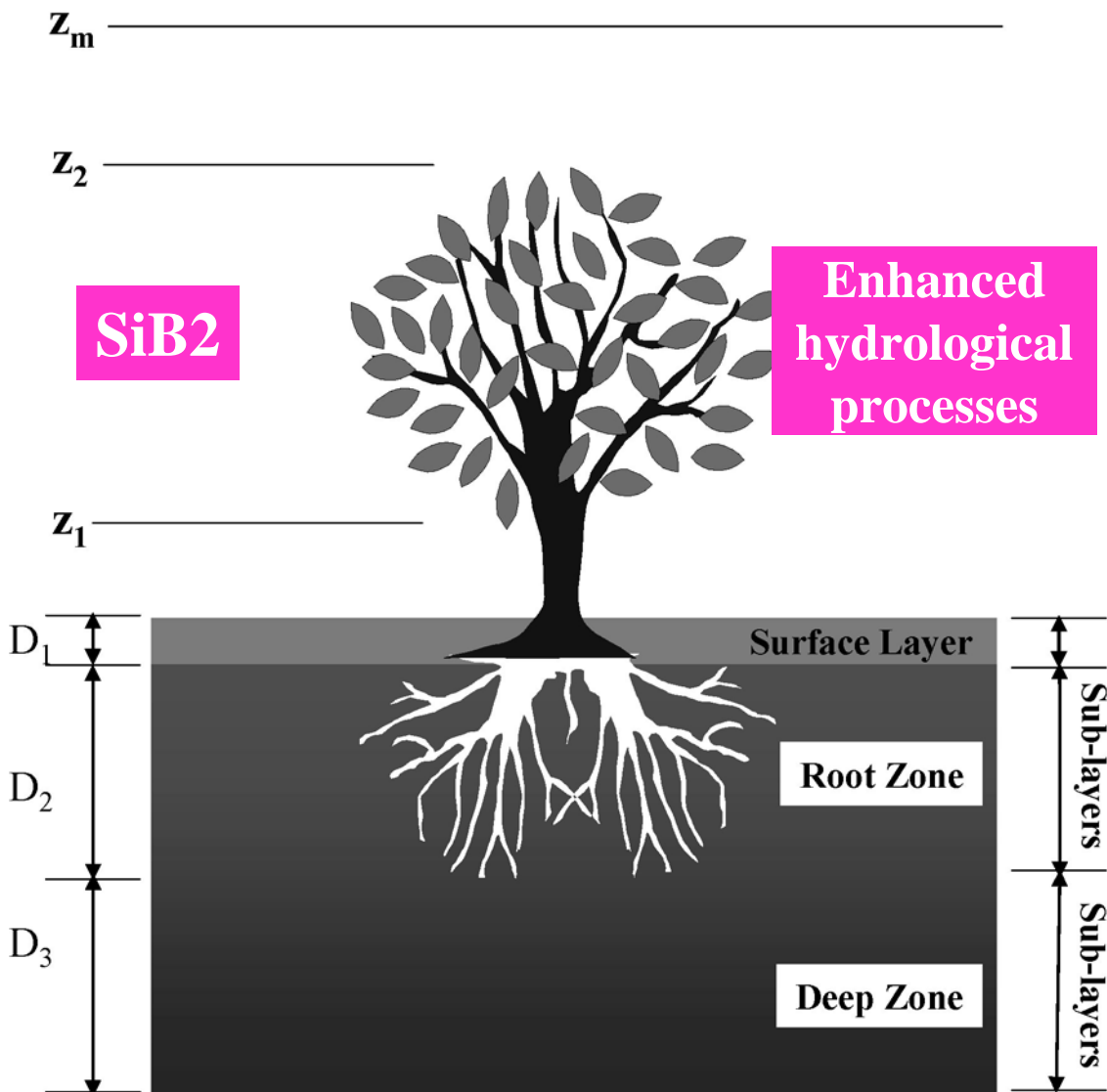
- porosity (saturated moisture)
- water retention:  $\theta-\phi$
- unsaturated hydraulic conductivity:  $k-\theta$

# Hydrologocally Enhanced Land-surface Model

1. Using distributed hydrological model;
2. Including radiation transfer processes;
3. Including biophysical processes;
4. Including biochemical processes.



# Hydrologically Enhanced Land-surface Process Model (HELP)



- (1) Using more reliable formulation for soil-water property by replacing the Campbell's formula with Von Genuchten's formula.
- (2) Using quasi 2-dimensional unsaturated zone model
- (3) Including the dynamic interaction between groundwater level and the unsaturated zone and the exchange between the groundwater and river.
- (4) Including surface routing along the hillslope.

## 10 soil layers:

- The first layer is fixed to be 0.05 m
- The root zone is subdivided
- The deep zone is subdivided

# Validation using the CEOP Thailand Site Observation

## ② Deciduous Forest

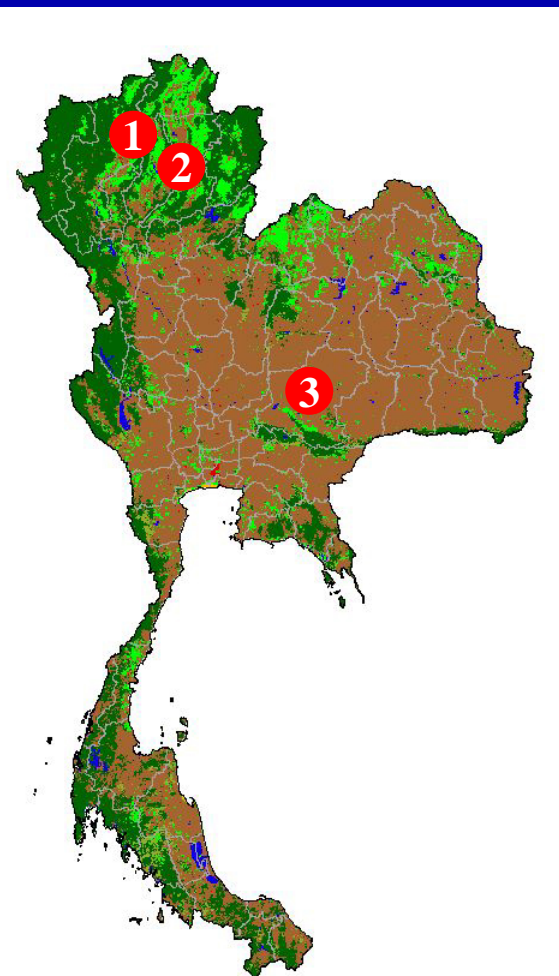


## ① Ever-green Forest

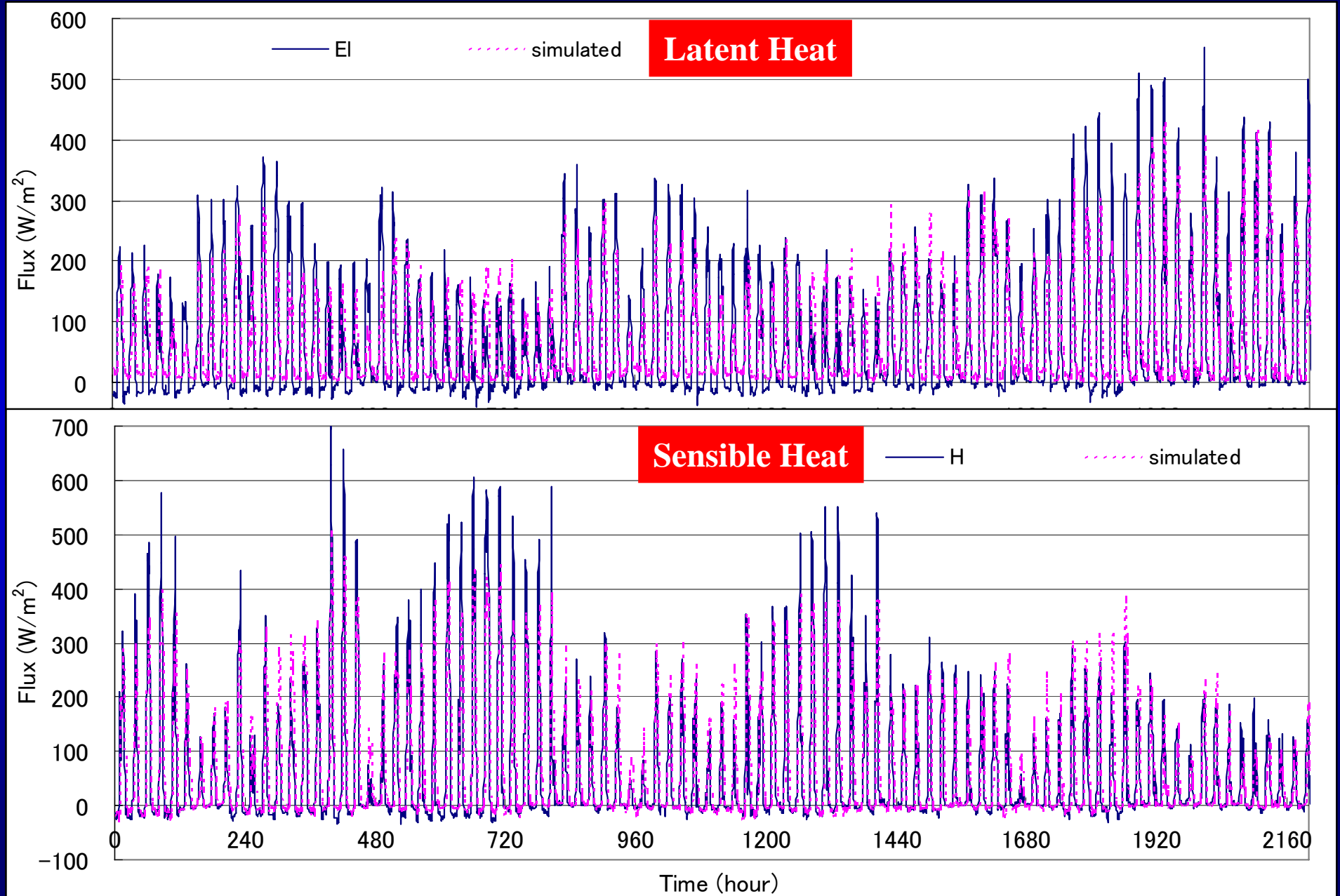


Kog-Ma Tower, Thailand.

## ③ Cassava

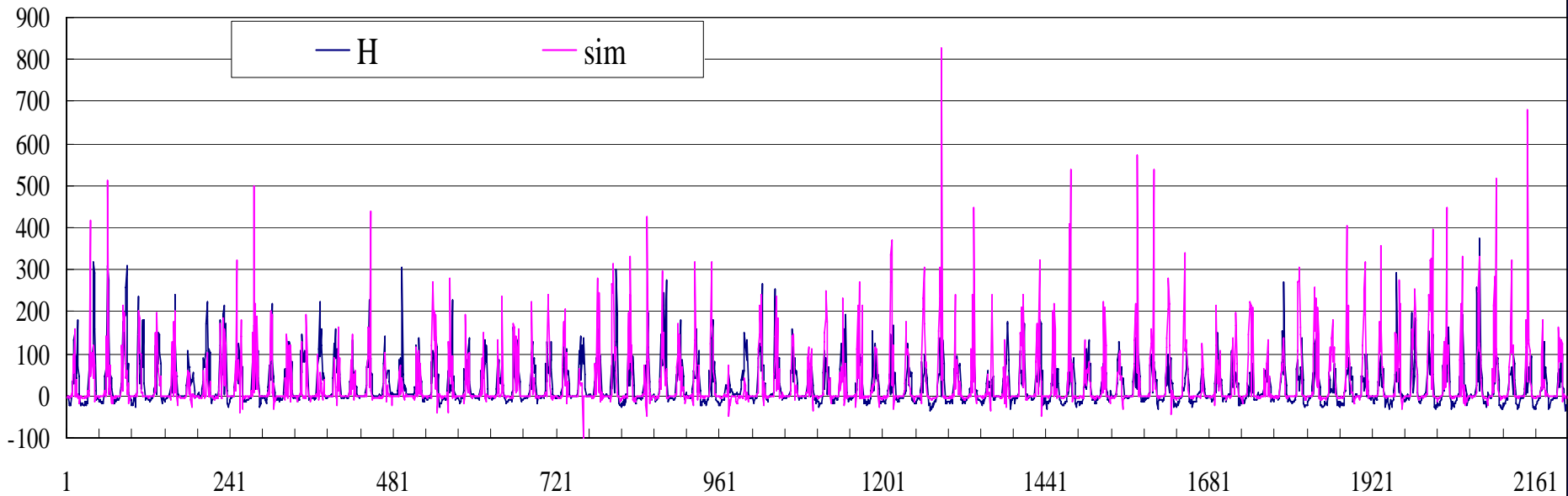
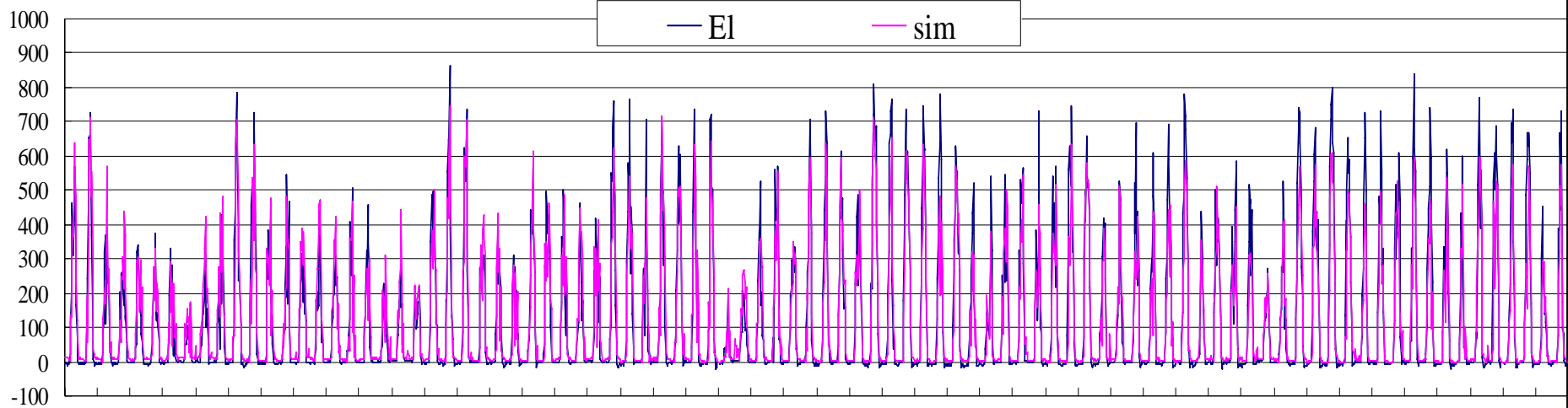


# Validation at one-D: the Cassava Site (July 2<sup>nd</sup> ~ Oct. 1<sup>st</sup>, 2001)

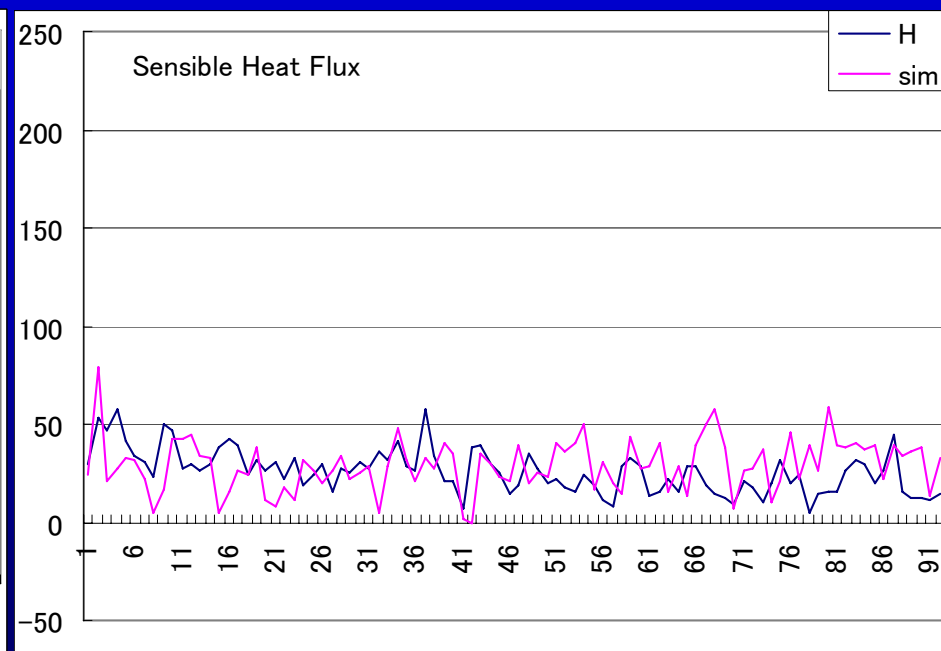
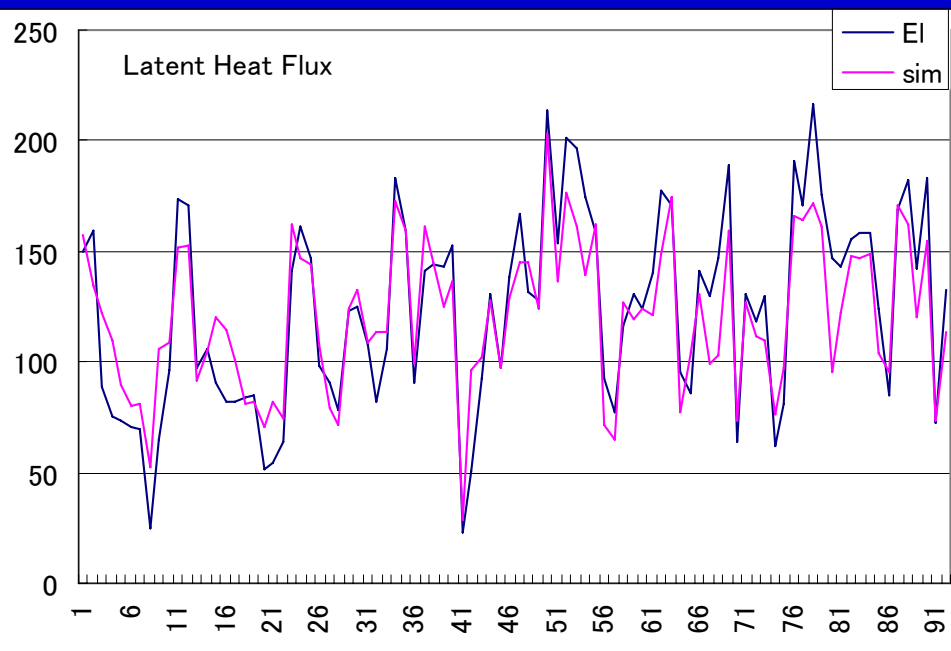
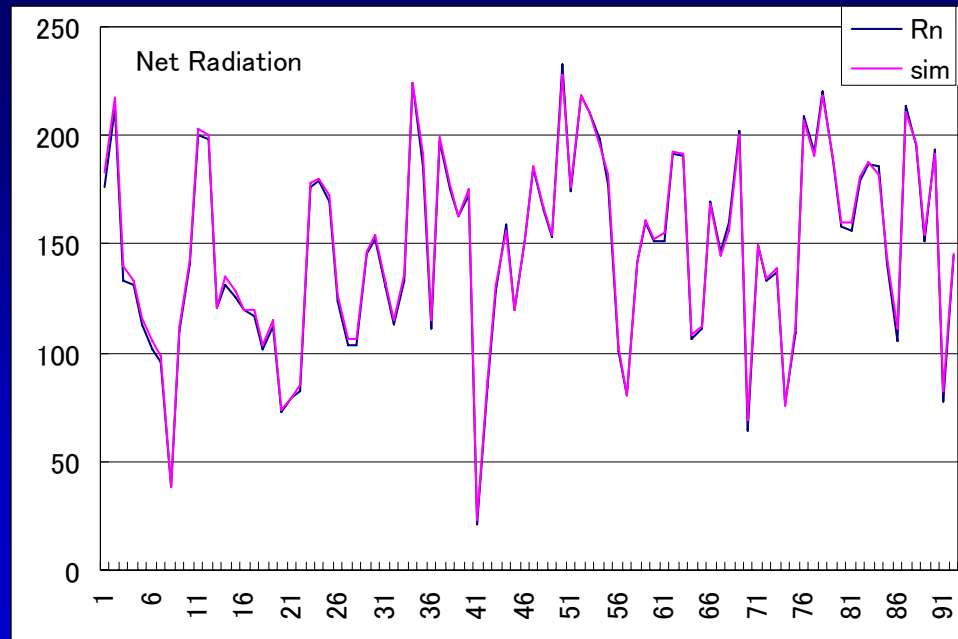




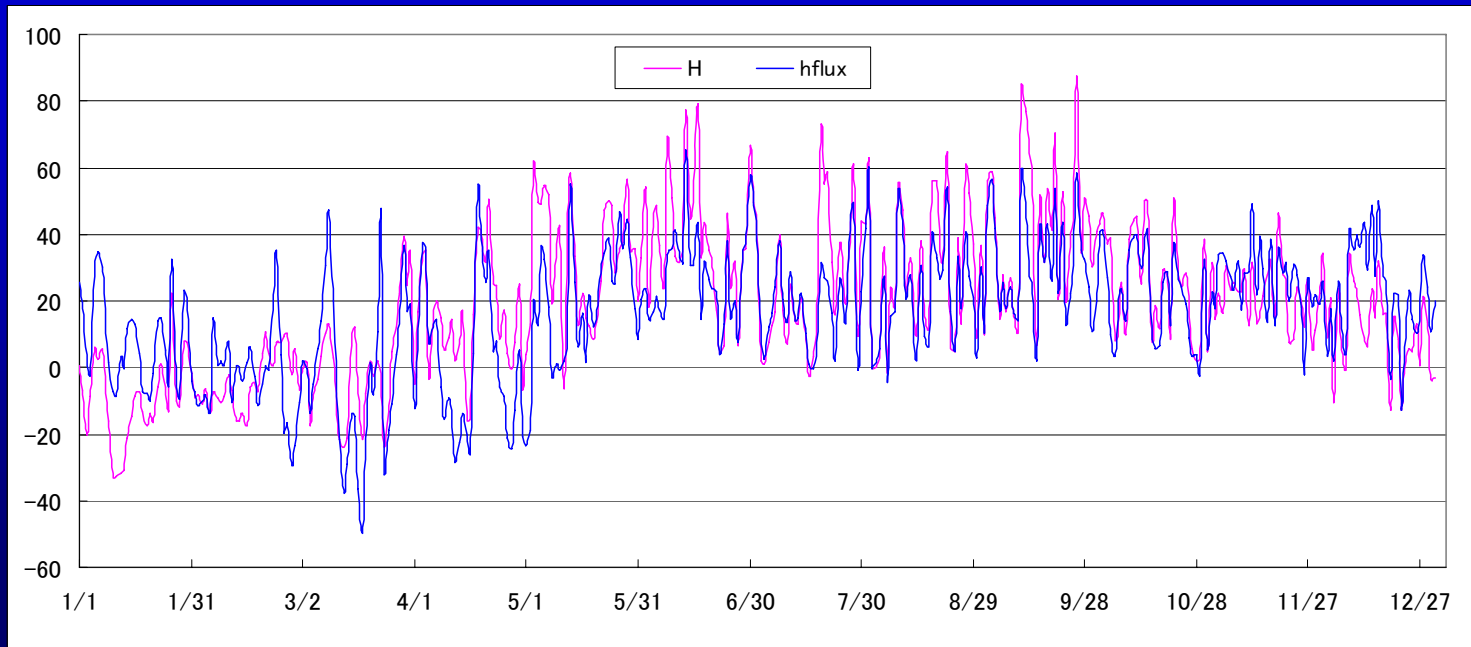
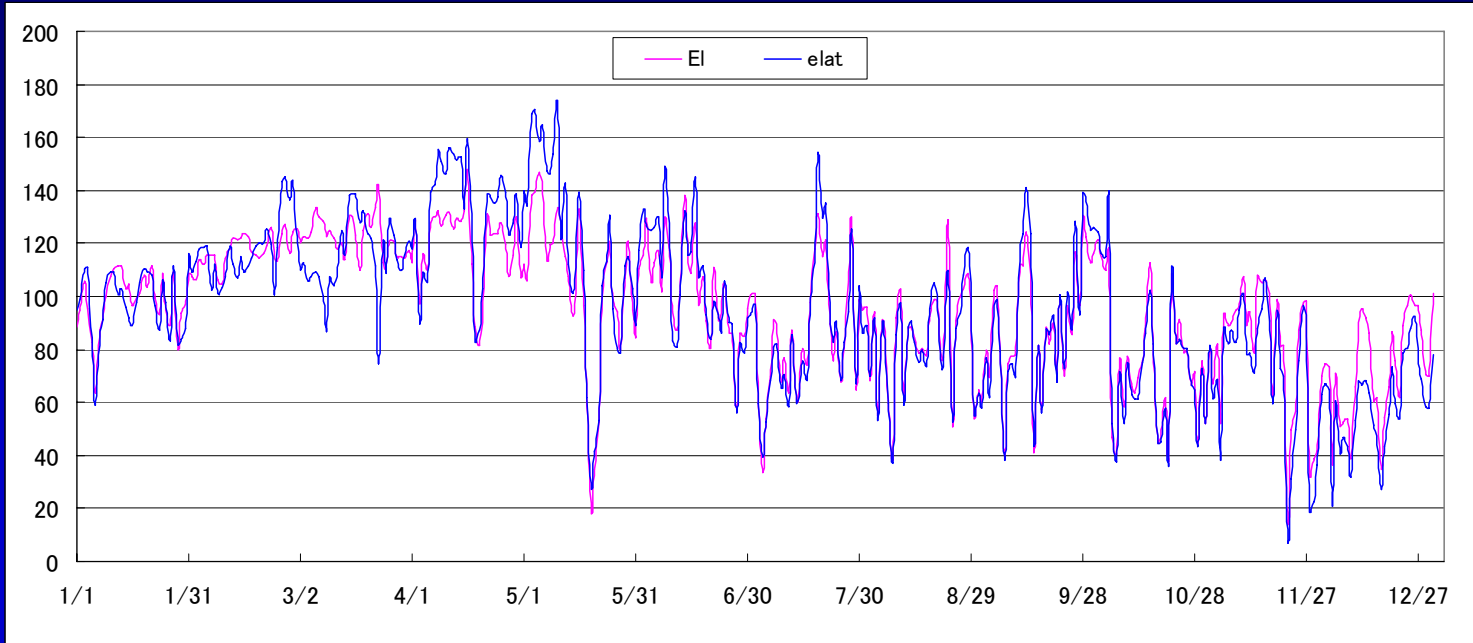
# Validation at one-D: the Deciduous Forest Site (July 2<sup>nd</sup> ~ Oct. 1<sup>st</sup>, 2001)



# Validation at one-D: the Deciduous Forest Site (July 2<sup>nd</sup> ~ Oct. 1<sup>st</sup>, 2001)



# Validation at one-D: the Deciduous Forest Site (Jan. 1<sup>st</sup> ~ Dec. 31<sup>st</sup>, 1998)





# Conclusion

- Soil - vegetation – atmosphere transfer processes could be the the key to simulating the water cycle specially in many water-stressed regions
- From the viewpoint of water resources management, it needs a basin-scale land surface model that can deal with the river discharge and groundwater flow
- The present research showed a potential possibility of developing a common Land Surface Model for more wider uses for atmospheric and hydrological purposes

**Thank You !**